

# HEATING OF "THIN" BODIES IN LIQUID MEDIA

L. S. Shvindlerman

Inzhenerno-fizicheskii zhurnal, Vol. 8, No. 1, pp. 53-57, 1965

Heating of "thin" ( $Bi \leq 0.25$ ) bodies in liquid media is examined, taking into account crystallization and fusion at the body-medium interface.

The medium considered is a fused salt and the heating system a salt melting bath. The ratio of the volume of the bath to that of the heated element is assumed to be such that introducing the element causes a negligible drop in bath temperature; the bath temperature is constant.

The temperature difference over the section of the element when heated (or cooled) is characterized by the parameter  $Bi = \alpha S / \lambda$ . Distinguishing thermally "thin" bodies (i.e., those in which the temperature drop over the section can be neglected [2]) by assigning a predetermined maximum temperature difference over the section, expressed in fractions of the initial temperature difference between the liquid and the metal, we get a definite value of the Bi number, which we can use as a conventional dividing line between "thin" and "massive" bodies. In engineering calculations relating to the heating of metal, "thin" bodies are characterized by  $Bi \leq 0.25$  [4].

Let us examine the heating of a flat element in a salt bath. The element may be regarded as a plane infinite wall, since two dimensions — length and width — greatly exceed the third — thickness. From the fact that the element is "thin," it follows that the temperature distribution in the element and in the film may be considered steady at any time (and, in particular, the temperature distribution in the film is linear). Heating in a salt bath is heating in a medium at a constant temperature [1, 2], but not heating at a constant surface temperature [3]. In fact, when the element is inserted into the bath, it draws heat from the surrounding fused salt and forms a layer of crystallized salt on its surface. The temperature distribution in the film, as we have noted already, is linear, increasing from the metal to the outer film surface. The latent heat of fusion of the salt and the heat it gives out in cooling from bath temperature to that of the film are acquired only by the metal. As the film grows, and the metal temperature accordingly increases, the temperature on the film outer surface increases until it reaches  $t_{fs}$ , thereafter remaining constant until the film has all fused.

Let us examine a layer of fused salt of thickness  $dx$  at distance  $x$  from the surface of the element. When the layer is cooled from temperature  $t_f$  to  $t_f - dt$ , the amount of heat given out is

$$dQ = -F \rho_s c_s dx dt. \quad (1)$$

We assume here, and in what follows, that the quantities  $\rho_m$ ,  $\rho_s$ ,  $c_m$ ,  $c_s$ , and  $\lambda_s$  are constant throughout the whole temperature interval studied. The error so introduced is not large, and it would not be difficult to allow for the dependence on temperature and phase state. The temperature distribution in the film obeys the equation

$$t_x = \frac{t_o - t_i}{\delta} x + t_i.$$

The amount of heat transferred to the metal by the salt in crystallizing is

$$Q_{tot} = Q_i + Q_f = - \int_{t_f}^{t_x} F \rho_s c_s dt \int_0^{\delta} d\delta + F \rho_s \delta \gamma_s$$

or

$$Q_{tot} = F \rho_s \delta c_s \left( t_f - \frac{t_i + t_o}{2} \right) + F \rho_s \gamma_s \delta.$$

Since all the heat released by the salt in crystallizing is transferred to the metal, we have

$$c_m m_m (t_m - t_{m0}) = F \rho_s \delta c_s \left( t_f - \frac{t_i + t_o}{2} \right) + F \rho_s \gamma_s \delta. \quad (2)$$

Fig. 1 gives a diagram of the thermal resistances of the system. The following equations may be derived from geometrical considerations:

$$\delta = \frac{\lambda_c}{\alpha_2} \frac{t_o - t_B}{t_f - t_o}, \quad (3)$$

$$\delta = \frac{\lambda_c}{\alpha_2} \left( \frac{t_o - t_m}{t_f - t_o} - \frac{\alpha_2}{\alpha_1} \right). \quad (4)$$

From (2)-(4) we can evaluate  $t_m$  and  $t_o$  as functions of  $\delta$ :

$$t_m = \frac{2(\theta + \varphi + \delta)(t_{m_0} + \beta\delta\gamma_s) + (2\theta + \delta)t_f\beta\delta c_s}{2(\theta + \varphi + \delta) + \beta\delta c_c(2\theta + \delta)};$$

$$t_H = \frac{2\theta t_{m_0} + 2\theta\beta\delta\gamma_s + 2\varphi t_f + 2\delta t_f + 2\theta\beta\delta c_s t_f + \beta\delta^2 c_s t_f}{2(\theta + \delta + \varphi) + \beta\delta c_s(2\theta + \delta)};$$

$$\theta = \frac{\lambda_s}{\alpha_2}; \quad \varphi = \frac{\lambda_s}{\alpha_1}; \quad \beta = \frac{F\rho_s}{c_m m_m} = \frac{F\rho_s}{c_m \frac{F}{S}\rho_m} = \frac{2\rho_s}{c_m S\rho_m}.$$

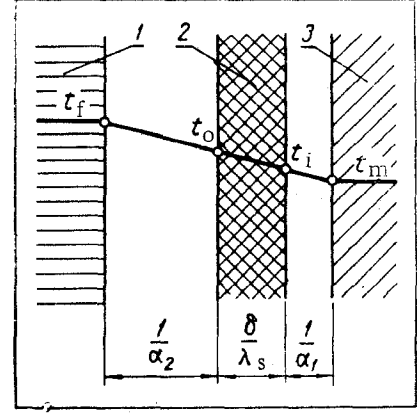


Fig. 1. Diagram of thermal resistances of system fused salt + heated body: 1 - fused salt; 2 - crystallized salt; 3 - metal element.

Putting  $t_o = t_{fs}$ , we obtain the maximum film thickness from (6)

$$\delta_0 = (-b + \sqrt{b^2 - 4al})/2a; \quad (6')$$

$$a = \beta c_s (t_f - t_{fs}) \cdot 1/2;$$

$$b = \theta\beta c_s (t_f - t_{fs}) + \theta\beta\gamma_s + t_f - t_{fs};$$

$$e = \varphi(t_f - t_{fs}) - \theta(t_{fs} - t_{m_0}).$$

It follows from (4) that the film will be completely fused ( $\delta = 0$ ) when the metal temperature  $t_{cfl} = t_{fs} - (t_f - t_o) \frac{\alpha_2}{\alpha_1}$ . If  $\alpha_1 \gg \alpha_2$  we have the trivial case  $t_m = t_{fs}$ .

Let us now find the growth time for the film. At any time  $\tau$  during growth, the amount of heat passing through the outer surface of the crystallized film in time  $d\tau$  is given by Newton's law:

$$dQ_g = F\alpha_2(t_f - t_o)d\tau.$$

This amount of heat may be represented as the amount of heat given up by a layer of crystallizing salt of thickness  $d\delta$  in cooling from  $t_f$  to  $t_o$ , plus the latent heat of fusion of the layer released in crystallizing:

$$F\alpha_2(t_f - t_o)d\tau = F\rho_s c_s (t_f - t_o)d\delta + F\rho_s \gamma_s d\delta \quad (7)$$

or

$$d\tau = \frac{\rho_s c_s}{\alpha_2} d\delta + \frac{\rho_s \gamma_s}{\alpha_2} \frac{d\delta}{t_f - t_o}. \quad (8)$$

By first substituting the value  $t_f - t_o$  from (6), and then integrating (8) in the limits 0 to  $\tau_g$  and 0 to  $\delta$ , we obtain the time taken for a film of thickness  $\delta$  to form. For  $\delta = \delta_0$ , we find the total time of film growth  $\tau_{g0}$ .

$$\tau_g = \left[ \frac{\rho_s(\theta + \varphi)}{\lambda_s \beta} + \frac{\rho_s(1 + \theta\beta c_s)(t_f - t_{m_0})}{\lambda_s \beta^2 \gamma_s} + \frac{\rho_s c_s (t_f - t_{m_0})^2}{2\lambda_s \beta^2 \gamma_s^2} \right] \ln \frac{t_f - t_{m_0}}{t_f - t_{m_0} - \beta\gamma_s \delta} - \left[ \frac{\rho_s c_s (t_f - t_{m_0})}{2\lambda_s \beta \gamma_s} + \frac{\rho_s}{\lambda_s \beta} \right] \delta - \frac{\rho_s c_s \delta^2}{4\lambda_s}. \quad (9)$$

To determine the fusion time of the film, we note that, after the temperature of the outer surface of the film has attained the fused salt temperature, the heat incident on the outer surface of the film in time  $d\tau$  will go to increase the metal temperature and the film temperature, and to transfer latent heat of fusion to the melting layer of the film  $d\delta$ .

$$F\alpha_2(t_f - t_o)d\tau = c_m m_m dt_m + F\rho_s c_s \delta d \left( \frac{t_o + t_i}{2} \right) - F\rho_s \gamma_s d\delta. \quad (10)$$

The last term is negative, since in this case the latent heat is absorbed.

Since  $t_0 = t_{fs}$  during the second period of the existence of the film, we may determine  $dt_i$  and  $dt_m$  from (3) and (4), and, substituting in (10), we have the differential equation for the film fusion time:

$$d\tau_{cf} = -\frac{\rho_s}{\theta\alpha_2\beta} d\delta - \frac{\rho_s c_s}{\alpha_2(\theta + \varphi)} \delta \frac{d\delta}{2} - \frac{\gamma_s \rho_s}{\alpha_2(t_f - t_{fs})} d\delta. \quad (11)$$

Integrating within the limits  $\tau_{g0}$  to  $\tau_{cf}$  and from  $\delta_0$  to  $\delta$ , we find the time required to melt the film from  $\delta_0$  to  $\delta$ :

$$\begin{aligned} \Delta\tau_{cf} &= \tau_{cf} - \tau_{g0} = \\ &= \left[ \frac{\rho_s}{\theta\alpha_2\beta} + \frac{\gamma_s \rho_s}{\alpha_2(t_f - t_{fs})} \right] (\delta_0 - \delta) + \frac{\rho_s c_s}{4\alpha_2(\theta + \varphi)} (\delta_0^2 - \delta^2). \end{aligned} \quad (12)$$

Putting  $\delta = 0$  we obtain the time for complete fusion of the film:

$$\tau_{cf,0} = \tau_{g0} + \left[ \frac{\rho_s}{\lambda_s \beta} + \frac{\gamma_s \rho_s}{\alpha_2(t_f - t_{fs})} \right] \delta_0 + \frac{\rho_s c_s}{4\alpha_2(\theta + \varphi)} \delta_0^2. \quad (13)$$

We see from (9) and (13) that the time of existence of the film, from the start of heating to the end of fusion is

$$\begin{aligned} \tau_{cf,0} &= \left[ \frac{\gamma_s \rho_s}{\alpha_2(t_f - t_{fs})} - \frac{\rho_s c_s (t_f - t_{m0})}{2\lambda_s \beta \gamma_s} \right] \delta_0 - \\ &\quad - \left[ \frac{\rho_s c_s}{4\lambda_s} \left( 1 - \frac{\alpha_1}{\alpha_1 + \alpha_2} \right) \right] \delta_0^2 + \\ &+ \left[ \frac{\rho_s(\theta + \varphi)}{\lambda_s \beta} + \frac{\rho_s(1 + \theta\beta c_s)(t_f - t_{m0})}{\lambda_s \beta^2 \gamma_s} + \frac{\rho_s c_s (t_f - t_{m0})^2}{2\lambda_s \beta^2 \gamma_s^2} \right] \ln \frac{t_f - t_{m0}}{t_f - t_{m0} - \beta \gamma_s \delta_0} \end{aligned}$$

The time for the element to be heated from  $t_{mcf}$  to  $t_{mf}$  may be determined from the known heating time of "thin" bodies, [1]:

$$\Delta\tau_f = \tau_{tot} - \tau_{cf,0} = \frac{\rho_M S c_M}{2\alpha_2} \ln \frac{t_f - t_{mcf}}{t_f - t_{mf}}. \quad (14)$$

The heat transfer coefficients  $\alpha_1$  and  $\alpha_2$  in (9), (13), and (14) are different, since they refer to different temperature intervals. This difference can be taken into account, but for simplicity we shall take average values of  $\alpha_1$  and  $\alpha_2$  over the whole temperature range in question,  $t_{m0}$  to  $t_{mf}$ .

Therefore, the time required for the element to be heated in the liquid from  $t_{m0}$  to  $t_{mf}$  is

$$\begin{aligned} \tau_{tot} &= \left[ \frac{\gamma_s \rho_s}{\alpha_2(t_f - t_{fs})} - \frac{\rho_s c_s (t_f - t_{m0})}{2\lambda_s \beta \gamma_s} \right] \delta_0 - \\ &\quad - \left[ \frac{\rho_s c_s}{4\lambda_s} \left( 1 - \frac{\alpha_1}{\alpha_1 + \alpha_2} \right) \right] \delta_0^2 + \\ &+ \left[ \frac{\rho_s(\theta + \varphi)}{\lambda_s \beta} + \frac{\rho_s(1 + \theta\beta c_s)(t_f - t_{m0})}{\lambda_s \beta^2 \gamma_s} + \frac{\rho_s c_s (t_f - t_{m0})^2}{2\lambda_s \beta^2 \gamma_s^2} \right] \ln \frac{t_f - t_{m0}}{t_f - t_{m0} - \beta \gamma_s \delta_0} + \\ &\quad + \frac{\rho_M c_M S}{2\alpha_2} \ln \frac{t_f - t_{mcf}}{t_f - t_{mf}}. \end{aligned} \quad (15)$$

The above calculation is correct for bodies that are "thin" from the thermal point of view. Since it also follows that the crystallized salt film must be thermally "thin" ( $Bi = \alpha_2 \delta_0 / \lambda_s \leq 0.25$ ), knowing  $\delta_0$  and  $Bi$ , we obtain the thickness  $S$  of the element on which a thermally "thin" film of thickness  $\delta_0$  is formed:

$$S \leq \frac{0,5 \rho_s}{c_M \rho_M} \left( \frac{\lambda_s}{\alpha_2} \right)^2 \frac{1,5 c_s (t_f - t_{fs}) + \gamma_s}{\frac{\lambda_s}{\alpha_2} (t_{fs} - t_{m0}) - \frac{\lambda_s}{\alpha_1} (t_f - t_{fs}) - 0,25 \frac{\lambda_s}{\alpha_2} (t_f - t_{fs})}. \quad (16)$$

For "thin" elements, moreover, we must have the relation  $Bi = \alpha_2 S / \lambda_m \leq 0.25$ . An element which is thermally "thin" for heating in a given liquid will have a thickness which satisfies both relationships. The above method of calculating heating times in liquids will be valid precisely for such elements.

To illustrate the results obtained, we shall calculate the heating time for an element with  $S = 2 \cdot 10^{-3}$  m. The medium is fused NaCl, with  $t_f = 1,273^\circ\text{K}$ ;  $t_{mf} = 1,173^\circ\text{K}$ ;  $t_{m_0} = 293^\circ\text{K}$ ;  $t_{fs} = 1,077^\circ\text{K}$  [5];  $\rho_s = 2,160 \text{ kg/m}^3$  [5];  $\rho_m = 7,800 \text{ kg/m}^3$  [2];  $\gamma_s = 5.15 \cdot 10^5 \text{ j/kg}$  [5];  $c_m = 0.5 \cdot 10^3 \text{ j/kg} \cdot \text{degree}$  [2];  $c_s = 0.88 \cdot 10^3 \text{ j/kg} \cdot \text{degree}$  [5];  $\lambda_m = 30.4 \text{ w/m} \cdot \text{degree}$  [2];  $\lambda_s = 1.12 \text{ w/m} \cdot \text{degree}$  [7];  $\alpha_2 = 350 \text{ w/m}^2 \cdot \text{degree}$  [2].

No accurate data on  $\alpha_1$  are given in the literature. We deduce from [7] that  $\alpha_1$  must be of the order  $1,163 \text{ w/m}^2 \cdot \text{degree}$ .

From (6'),  $\delta_0 = 0.574 \cdot 10^{-3}$  m; for the element  $Bi = 1.15 \cdot 10^{-2} \leq 0.25$ ; for the film  $Bi = 0.18 < 0.25$ ;  $\tau_{\text{tot}} = 43.9 \text{ sec}$ .

Practical recommendations as regards the heating time for rectangular elements in salt baths at such temperatures [8] indicate a value of  $\tau_{\text{tot}}$  of 18-22 sec. for a 1 mm section, which agrees reasonably with the calculated value.

#### NOTATION

$\alpha_1$  and  $\alpha_2$  – heat transfer coefficients for film/metal and fused salt/metal (or fused salt/film);  $\lambda_m$  and  $\lambda_s$  – thermal conductivity of metal and crystallized salt;  $t_f$ ,  $t_{fs}$ ,  $t_o$  and  $t_i$ ,  $t_{m_0}$  and  $t_{mf}$  – temperatures of: medium or fused salt, fusion of salt, outer and inner film surface, metal – initial and final;  $s$  – calculated thickness of element;  $F$  – surface area of element;  $m$  – mass of element;  $\rho_m$  – density of metal;  $\rho_s$  – density of crystallized salt;  $c_m$  and  $c_s$  – specific heat capacity of metal and salt;  $\delta$  – thickness of film of crystallized salt;  $\gamma_s$  – latent heat of fusion of salt.

#### REFERENCES

1. A. L. Nemchinskii, Thermal Calculations Relating to Heat Treatment [in Russian], Sudpromgiz, 1951.
2. K. N. Sokolov, Heat Treatment Equipment [in Russian], Mashgiz, 1957.
3. A. A. Shmykov, Heat Manual [in Russian], Mashgiz, 1961.
4. G. P. Ivantsov, Heating of Metal [in Russian], Metallurgizdat, 1948.
5. Concise Engineering Physics Handbook (ed. K. P. Yakovlev) [in Russian], 1, Fizmatgiz, 1960.
6. Chemistry Handbook [in Russian], 1, Goskhimizdat, 1963.
7. Yu. P. Shlykov and E. A. Ganin, Contact Heat Transfer [in Russian], Gosenergoizdat, 1963.
8. I. S. Kamenichnii, Concise Handbook of Heat Technology [in Russian], Mashgiz, 1963.

21 April 1964

Institute of Structural Design and Planning  
Sovnarkhoz UkrSSR, Kiev.